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Evaluation of air-particle abrasion of Y-TZP with different particles using microstructural analysis

Turp, V ; Sen, D ; Tuncelli, B ; Goller, G ; Özcan, M

Abstract: BACKGROUND: This study evaluated the effect of air-particle abrasion with different particle sizes on the surface roughness and phase transformation of yttria-stabilized tetragonal zirconia ceramics (Y-TZP). **METHODS:** Eighty-four Y-TZP discs of 15 mm diameter and 1.0 mm thickness were fabricated. The samples were divided into four groups (n = 21): (1) air-particle abrasion with 30 µm CoJet sand blast coating agent (CoJet, 3M ESPE); (2) 50 µm Al₂O₃ particles; (3) 110 µm Al₂O₃ particles; and (4) 250 µm Al₂O₃ particles. Each group was further divided into three subgroups each (n = 7) and treated for 5 seconds, 15 seconds and 30 seconds. Mean surface roughness was determined using a profilometer. The surfaces were analysed with a scanning electron microscope. XRD analysis was employed and the relative amount of the monoclinic phase was calculated. The results were statistically analysed by two-way analysis of variance (ANOVA, p < 0.05). **RESULTS:** Air-particle abrasion with 250 µm Al₂O₃ particles for 30 seconds had the highest surface roughness (p < 0.001) and a significantly higher amount of monoclinic phase compared to air-particle abrasion with 30 µm, 50 µm and 110 µm particles (p < 0.001). **CONCLUSIONS:** Duration and particle size of air-particle abrasion affects the roughness and phase transformation of Y-TZP. Longer treatment times with larger particles may result in degradation of material.

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Effect of particle size and deposition duration of air-particle abrasion on the surface properties and microstructure of zirconia

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Short Title: Air-particle abrasion effect on zirconia

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ABSTRACT

Background: This study evaluated the effect of particle size and deposition duration of air-particle abrasion on the surface properties and microstructure of zirconia.

Methods: Zirconia discs (N=84) (diameter: 15 mm, thickness: 1 mm) (Cercon, Degudent) were polished and randomly divided into 4 groups (n=21). Specimens were subjected to air-particle abrasion with a) 30 μm SiO_2 (CoJet, 3M ESPE), b) 50 μm Al_2O_3 particles, c) 110 μm Al_2O_3 particles and d) 250 μm Al_2O_3 particles for a duration of 5, 15 and 30 seconds (n=7 per subgroup). Surface roughness was measured using a 3D profilometer and the relative amount of monoclinic phase was calculated using XRD. Specimen surfaces were also analyzed under SEM. Data were statistically analyzed by 2-way ANOVA and Tukey's test ($\alpha=0.05$).

Results: Air-particle abrasion with 30 μm SiO_2 created significantly less surface roughness (0.57 ± 0.04 - 0.69 ± 0.1 μm) than those of other particle types at all deposition durations ($p<0.001$). The highest roughness was observed with 250 μm Al_2O_3 particles after 30 seconds deposition (1.16 ± 0.2 μm) ($p<0.001$). The highest amount of monoclinical phase was observed with 250 μm Al_2O_3 particles after 30 seconds (16.43%) compared to other groups (9.11 - 15.6%) ($p<0.001$).

Conclusions: Increase in particle size from 30 to 250 μm and deposition duration from 5 to 30 seconds during air-particle abrasion, enhances surface roughness and monoclinical phase of zirconia.

Keywords: Aging, air-particle abrasion, Y-TZP, XRD analysis, zirconia, surface roughness

INTRODUCTION

High aesthetic demands of patients and biocompatibility requirements have increased the use of all-ceramic systems in dentistry. A major problem with all-ceramic systems is the low fracture resistance. Yttria-stabilized tetragonal zirconia polycrystal (hereon: zirconia) is employed as framework materials for fixed dental prosthesis (FDP) in prosthodontics or as implant material due to their high strength and toughness.¹ Zirconia frameworks for FDPs are fabricated using the CAD/CAM systems as a standard routine.²

Pure zirconia has a monoclinic crystal structure at room temperature and transitions to tetragonal and cubic phase at increasing temperatures.³ The volume expansion caused from cubic to tetragonal and tetragonal to monoclinic phase transformation induces high stresses that may cause pure zirconia to crack upon cooling from high temperatures. Several different oxides such as magnesium oxide, yttrium oxide, calcium oxide, and cerium oxide are added to zirconia to stabilize the tetragonal and/or cubic phases. Among all phases, tetragonal phase is metastable. Compared to the other dental ceramics, zirconia has superior mechanical properties due to the transformation toughening mechanism.⁴ When sufficient quantity of the metastable tetragonal phase is present, then an applied stress, magnified by the stress concentration at a crack tip, can cause the tetragonal phase to convert to monoclinic.⁴ This results in a volume expansion. Phase transformation can then put the crack into compression, retarding its growth, and enhancing the fracture toughness. This mechanism is known as transformation toughening, and significantly extends the reliability and lifetime of products made with stabilized zirconia.^{3,4}

During laboratory or chairside procedures such as grinding, polishing or surface conditioning with abrasives, commonly performed by dental technicians and clinicians, internal stresses may cause phase transformation in the material. Air-particle abrasion is reported to be a requirement in order to achieve sufficient adhesion between the adhesive resin cements and zirconia ceramics.⁵⁻⁸ Air-abrasion systems rely on the deposition of different particle types and sizes ranging between 30 to 250 μm .^{9,10} The abrasion process removes the uppermost contaminated loose layers and the roughened surface provides some level of mechanical retention with the adhesive resin cement.^{9,10} However, the knowledge as to whether using large or small particle size to increase resin bond to high-strength ceramics of different

microstructures and chemical compositions is limited.^{11,12} Furthermore, to the authors' best knowledge the possible effect on the transformation change as a function of deposition duration has not been studied.

The objectives of this study therefore, were to evaluate the effect of particle size and deposition duration of air-particle abrasion on the surface properties and microstructure of zirconia. The null hypothesis tested was that particle type and deposition duration would not affect the surface morphology, roughness and phase transformation of zirconia.

MATERIALS AND METHODS

Specimen preparation

Zirconia discs (N=84) (diameter: 15 mm, thickness: 1 mm) were fabricated from non-HIPPED Cercon blocks (Cercon, Degudent, Hanau, Germany). They were sintered to full density in a furnace, according to the manufacturer's instructions and polished under water to the final thickness of 1 ± 0.13 mm with 320-, 400-, 600-, and 1200-grit SiC papers (Struers, Ballerup, Denmark) using a polishing machine (LaboPol-5, Struers, Ballerup, Denmark).

Zirconia discs were then randomly divided into 4 groups (n=21). Specimens were subjected to air-particle abrasion with a) 30 μm SiO_2 (CoJet, 3M ESPE, Seefeld, Germany), b) 50 μm Al_2O_3 particles (Korox, Bego, Bremen, Germany), c) 110 μm Al_2O_3 particles (Korox) and d) 250 μm Al_2O_3 particles (Korox) for a duration of 5, 15 and 30 seconds (n=7 per subgroup) at 2 bar pressure from a distance of approximately 10 mm (Easyblast, BEGO, Bremen, Germany).

Surface roughness measurement

After air-abrasion protocols, surface roughness of zirconia specimens were measured using a 3D optical profilometer (Veeco NT1100, Veeco, New York, USA). Non-contact, white-light vertical interferometer was used to measure the roughness of the assessed profile (R_a) using following parameters: magnification: 5.12x, sampling: 1.64 μm , array size: 736x480. Three measurements were made with a travelling distance of 2 mm across the treated surface of the specimens, and the mean value was calculated for each group. 3D images were captured using the software of the equipment (Wyko Vision 32, New York, USA).

X-Ray Diffraction and SEM analysis

The relative amount of monoclinic phase of zirconia as a function of particle type and deposition duration was calculated using X-ray diffraction analysis (X'pert Pro PANalytical, Almelo, The Netherlands). The calculations were based on the method of Garvie and Nicholson, according to the formula:¹³

$$X_m = [I_m(-111) + I_m(111)] / [I_m(-111) + I_m(111) + I_t(101)]$$

where X_m is the mass fraction of monoclinic phase, $I_m(-111)$ is the intensity of monoclinic peak at 28.2° , $I_m(111)$ is the intensity of monoclinic peak at 31.5° and $I_t(101)$ is the intensity of monoclinic peak at 30.2° .

Monoclinic phase volume percentage (V_m) was calculated using formula of Toraya et al.¹⁴

$$V_m = 1.311 X_m / (1 + 0.311 X_m)$$

where V_m is the monoclinic phase volume percentage and X_m is the mass fraction of monoclinic phase.

The surfaces of the 30 second treated specimens were further evaluated using Scanning Electron Microscope (SEM, JSM 7000F, JEOL, Japan) at x700 magnification.

Statistical analysis

Statistical analysis was performed using the software Statistix 8.0 for Windows (Analytical Software Inc, Tallahassee, FL, USA). The surface roughness data (μm) and relative amount of the monoclinic phase were submitted to two-way analysis of variance (2-way ANOVA) separately with the particle types (4 levels; 30, 50, 110, 250 μm particles) and deposition durations (3 levels; 5, 15, 30 seconds) as independent variables. Multiple comparisons were made using Tukey's test. P values less than 0.05 were considered to be statistically significant in all tests.

Results

Particle type ($p < 0.001$) and air-abrasion deposition duration ($p < 0.001$) had a significant effect on the surface roughness of zirconia. Interaction terms were also significant ($p < 0.001$).

Except 30 μm SiO_2 group, there was no statistically significant difference in surface roughness between subgroups after 5 seconds of deposition. As the deposition duration increased, the mean roughness values increased significantly ($p < 0.001$) (Table 1).

Air-particle abrasion with 30 μm SiO_2 created significantly less surface roughness (0.57 ± 0.04 - 0.69 ± 0.1 μm) than those of other particle types at all deposition durations ($p<0.001$). There was no significant difference between 5 and 15 seconds of 30 μm SiO_2 deposition ($p>0.001$) but 30 seconds subgroup created significantly higher roughness ($p<0.001$).

The highest roughness was observed with 250 μm Al_2O_3 particles after 30 seconds deposition (1.16 ± 0.2 μm) ($p<0.001$).

Particle type ($p<0.001$) and air-abrasion deposition duration ($p<0.001$) had a significant effect on the relative amount of monoclinical phase. Interaction terms were also significant ($p<0.001$).

The highest relative amount of monoclinical phase was observed with 250 μm Al_2O_3 particles after 30 seconds (16.43 ± 0.33 %) compared to other groups ($p<0.001$) (Table 2). Deposition duration of 30 μm SiO_2 did not affect the monoclinic phase significantly ($p>0.001$). For the 50 and 110 μm particles, 30 seconds of deposition increased the monoclinic phase significantly compared to 5 and 15 seconds ($p<0.001$). The XRD diagrams for each group are presented in Figs. 1a-d. Tetragonal and monoclinic peaks can be observed in the diagrams.

The 3D profilometry images displayed an increase in surface roughness and irregularities of the surface with the increase in the particle size and deposition duration but the traces of hard-machining were not completely removed even after 30 seconds (Figs. 2a-d). However, it can be observed that grooves and valleys on the surface are flattened as the application duration increased.

SEM images indicated grooves and scratches after 30 seconds of deposition with all particle sizes (Figs. 3a-d). Major qualitative differences were not observed in SEM imagery, hard machining traces were present in all groups.

DISCUSSION

Zirconia ceramics seem to be able to withstand high chewing forces but establishing adhesion of the luting cement to this ceramic is a critical issue for their clinical success.^{5,6,15-17} Although there is not a specific cementation protocol supported by clinical evidence for zirconia FDPs,^{7,18} the recommended approach is the use of resin cements in combination with surface treatments.¹⁹ Unfortunately, zirconia is affected by

several conditioning methods applied to its surface during common stages of manufacturing and clinical adjustment of the restoration, such as hard-machining, grinding and air-particle abrasion.²⁰ Among these, air-particle abrasion has been reported to be a prerequisite for achieving sufficient bond strength between zirconia and resin cement.^{6,8,21}

Air-abrasion systems are typically based on deposition of particles ranging between 30 to 250 μm on the material's surface under pressure.^{10,22} The increase in roughness also forms a larger surface area for the retention of the resin cement. However, there is limited knowledge as to whether micromechanical retention using large or small particle size results in degradation of the mechanical properties of zirconia.²¹ Therefore, this study was undertaken to evaluate the effect of particle size and deposition duration of air-particle abrasion on the surface properties and microstructure of zirconia. Since the surface roughness results and the relative amount of monoclinical phase varied as a function of particle size and deposition duration, the null hypothesis tested was rejected.

Air-particle abrasion is in fact a gentle conditioning process compared to other surface treatments.¹⁶ The abrasion and heat produced by air-particle abrasion is considerably less compared to hard machining and grinding and it has been reported in several studies that the strength of the material could even increase after the air-abrasion process.^{22,23} In this study, as the particle size and application duration increased, the significant increase in monoclinic phase was observed.^{20,23} This may be resulting from an excess t-m transformation on the surface of the specimens. Hence, it can be anticipated that air-particle abrasion may lose its positive effect due to increase in duration of application and particle size. In principle, air-particle abrasion is used to clean and achieve micromechanical retention on the ceramic surface. However, the application duration or the particle size may change depending on the clinical objectives. For this reason, in this study 5, 15 and 30 seconds of deposition was chosen. Among specimens treated for 5 seconds, 30 μm SiO_2 group showed statistically less surface roughness and monoclinical phase compared to those of other 50, 110 and 250 μm Al_2O_3 . The so-called CoJet sand is basically ordinary alumina particles coated with silica using the sol-gel technology. With all particle types, 5 seconds of deposition seem to create the least damage on zirconia. Yet, considering the hard surface of zirconia, one can argue whether 5 seconds would be sufficient to achieve a clean, microretentive surface for sufficient adhesion. Also, surface area of

the restoration dictates the necessity for longer deposition duration. Nevertheless, as the duration increased, significant differences in surface roughness were observed depending on the particle size. With the increase in particle size increased, the surface irregularities also increased, supported by the profilometry images and measurements. However, a flattening of surface was observed in the topographic profilometry images while the surface roughness was increased. According to this result it can be speculated that although wide valleys and grooves are leveled by air-particle abrasion, roughness increases on the smaller areas where measurements are read.

The increase in monoclinic phase was parallel with surface roughness measurements in all groups, being more prominent for 110 and 250 μm Al_2O_3 . This phenomenon was attributed to tetragonal to monoclinic phase transformation on the zirconia surface, resulting in grain push-out and thereby, increased surface roughness.¹¹ Excessive tetragonal to monoclinic phase transformation may affect the mechanical properties of the zirconia negatively and result in degradation of this ceramic.¹¹ Kosmac et al. observed zirconia layers after air-particle abrasion with 110 μm particles. They reported the formation of a thin compressive surface layer and surface cracks that do not exceed this zirconia layer. They stated that the thickness of this layer is the similar to the size of an average zirconia grain, and it even increases the strength of the material by initiating transformation when confronted with stress.^{20,23} The changes in the compressive surface layer may be important as it may be affected by longer deposition durations. The findings of this study support this phenomenon.

According to the current information, the maximum acceptable amount of monoclinic phase in zirconia is 25 per cent.^{24,25} The amount of monoclinic phase after 250 μm Al_2O_3 particle deposition for 15 and 30 seconds (15.63% and 16.43%, respectively) did not exceed this limit. Also, SEM images verified that the grooves and traces of hard-machining were not completely removed after 30 seconds of air-particle abrasion, regardless of the grain size. In a previous study, it was reported that air-particle abrasion with 50 μm Al_2O_3 increased the strength of zirconia by removing the weak grains and grinding traces, whereas 120 μm Al_2O_3 weakened this ceramic, as the latter created new surface flaws.²⁶ Sato et al. used 125- μm silicon carbide and 70- μm alumina Al_2O_3 for air-particle abrasion and reported that biaxial flexural strength of zirconia increased by the stress-induced transformation with high monoclinic phase content.²⁷

However, they also reported that excess phase transformation that took place after silicon carbide air-particle abrasion decreased the biaxial flexural strength.²⁷ Thus, future studies should not only report on the particle size used but also the deposition duration and pressure should be mentioned as it may relate to the formation of a better compressive layer.

Until it is clinically proven whether air-abrasion contributes to degradation of zirconia, clinicians should apply air-particle abrasion as short as possible and use preferably particles with less sharp morphologies. Further studies are recommended look at the longer deposition durations of air-particle abrasion on microstructure and mechanical properties of zirconia.

CONCLUSIONS

The increase in particle size and deposition duration during air-abrasion protocols enhanced the surface roughness and monoclinic phase transformation of the tested zirconia.

Disclosure

The authors declare that they have no conflict of interests.

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Captions to tables and figures:

Tables:

Table 1. Mean surface roughness (R_a , μm) and standard deviations of zirconia specimens as a function of particle type and deposition duration. Same superscript capital letters indicate no significant difference in the same row, and small letters in the same column ($p < 0.05$)

Table 2. Relative amount of monoclinical phase (%) according to XRD measurements. Same superscript capital letters indicate no significant difference in the same row, and small letters in the same column ($p < 0.05$)

Figures:

Figs. 1a-d XRD diagrams of zirconia specimens after deposition of **a)** 30 μm SiO_2 , **b)** 50 μm Al_2O_3 , **c)** 110 μm Al_2O_3 and **d)** 250 μm Al_2O_3 for 5, 15 and 30 seconds. Note the differences in T and M peaks as the application duration changes.

Figs. 2a-d 3D profilometry images of zirconia specimens after deposition of **a)** 30 μm SiO_2 , **b)** 50 μm Al_2O_3 , **c)** 110 μm Al_2O_3 and **d)** 250 μm Al_2O_3 for 5, 15 and 30 seconds. Note that the hard-milling traces were not completely removed in all groups.

Figs. 3a-d SEM images (x700) of zirconia specimens after deposition of **a)** 30 μm SiO_2 , **b)** 50 μm Al_2O_3 , **c)** 110 μm Al_2O_3 and **d)** 250 μm Al_2O_3 for 30 seconds. Note that the hard-milling traces were not completely removed in all groups.

Tables

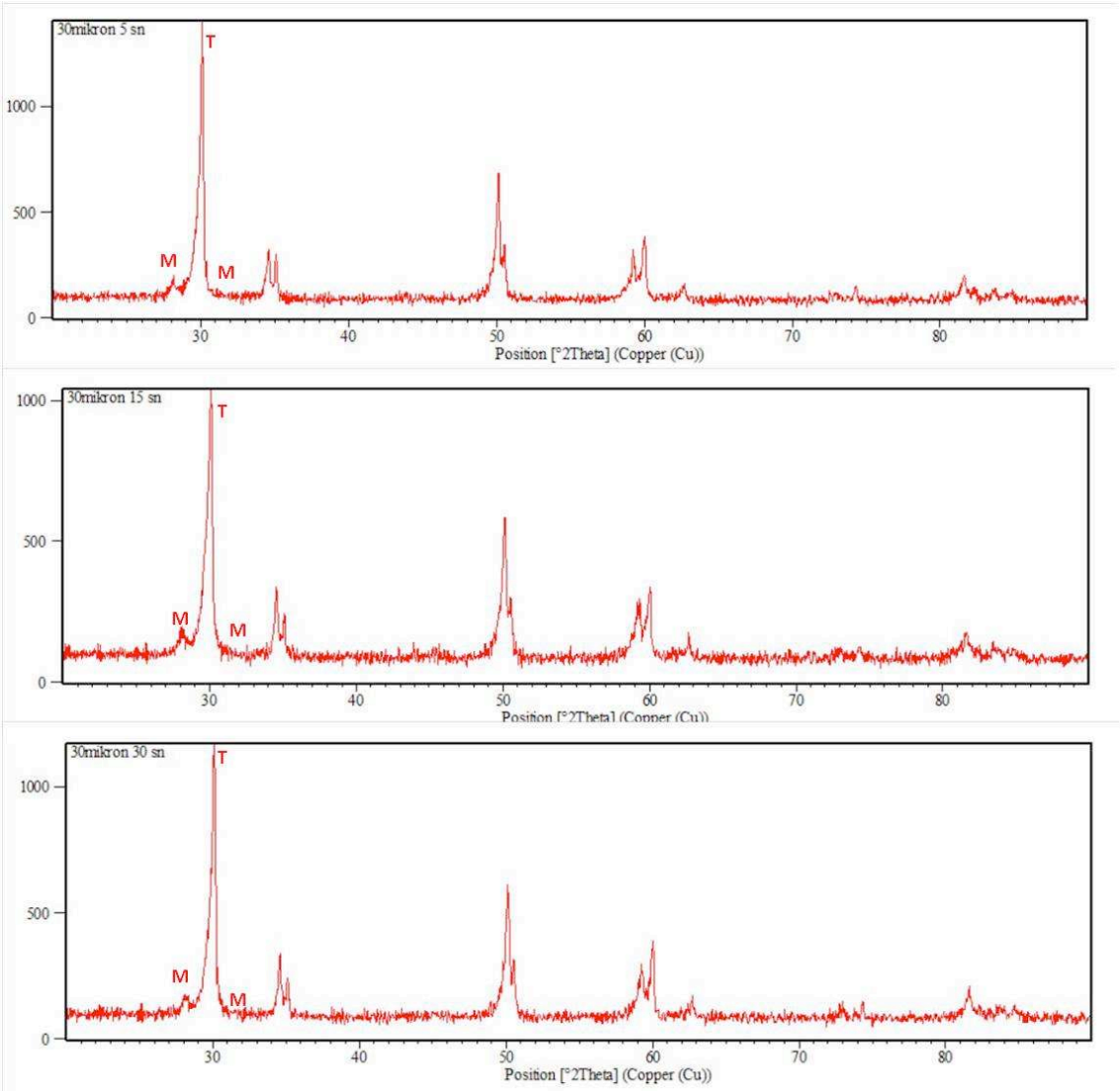
	5 seconds	15 seconds	30 seconds
30 μm SiO_2	$0.57 \pm 0.04^{\text{A},\text{a}}$	$0.62 \pm 0.12^{\text{A},\text{a}}$	$0.69 \pm 0.11^{\text{B},\text{a}}$
50 μm Al_2O_3	$0.80 \pm 0.13^{\text{A},\text{b}}$	$0.87 \pm 0.14^{\text{B},\text{b}}$	$0.94 \pm 0.18^{\text{C},\text{b}}$
110 μm Al_2O_3	$0.82 \pm 0.14^{\text{A},\text{b}}$	$0.91 \pm 0.21^{\text{B},\text{c}}$	$1.10 \pm 0.11^{\text{B},\text{c}}$
250 μm Al_2O_3	$0.83 \pm 0.16^{\text{A},\text{b}}$	$0.93 \pm 0.18^{\text{B},\text{c}}$	$1.16 \pm 0.18^{\text{C},\text{d}}$

Table 1. Mean surface roughness (Ra, μm) and standard deviations of zirconia specimens as a function of particle type and deposition duration. Same superscript capital letters indicate no significant difference in the same row, and small letters in the same column ($p < 0.05$)

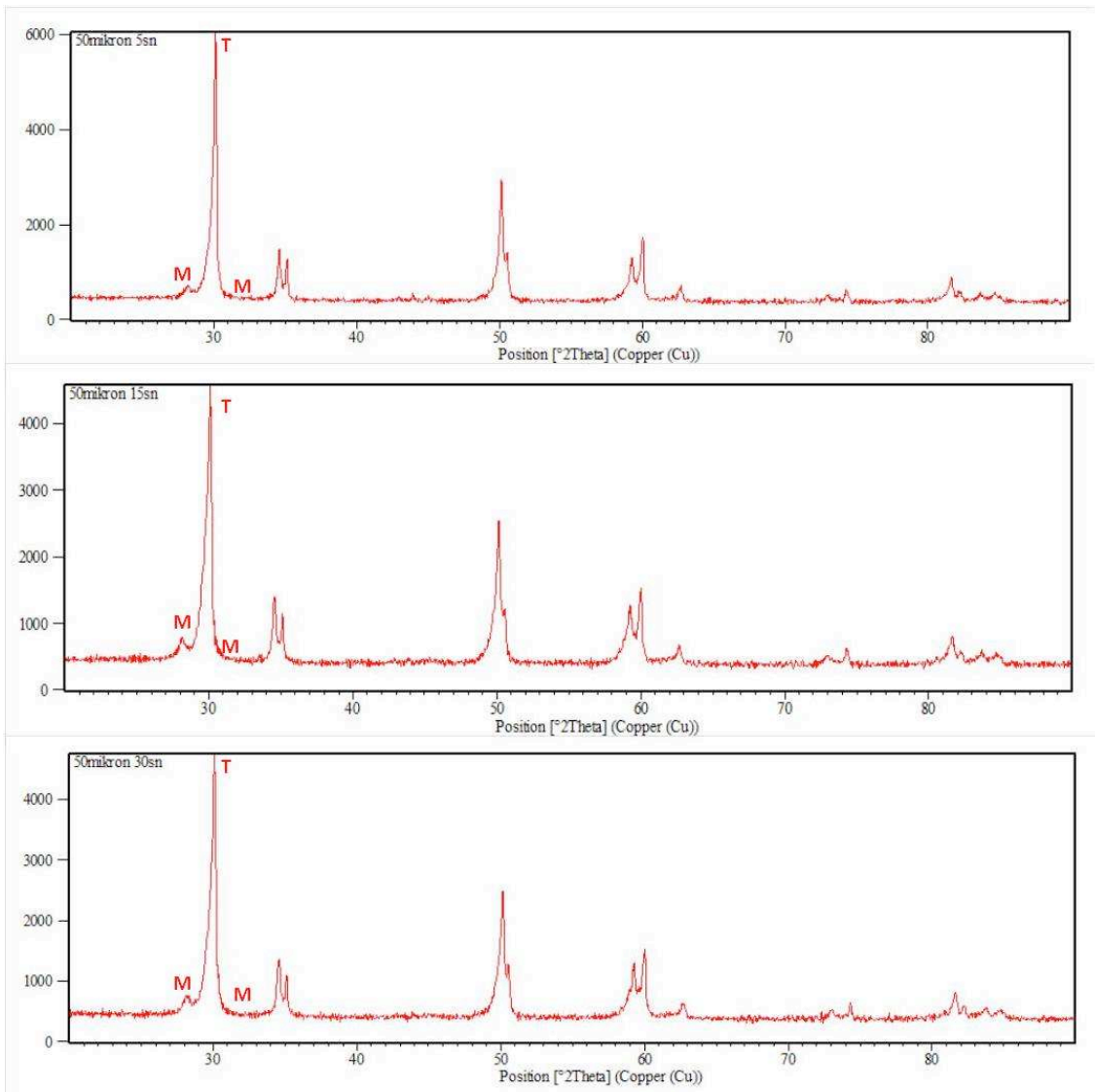
	5 seconds	15 seconds	30 seconds
30 μm SiO_2	$8.91 \pm 0.23^{\text{A},\text{a}}$	$9.03 \pm 0.32^{\text{A},\text{a}}$	$9.11 \pm 0.15^{\text{A},\text{a}}$
50 μm Al_2O_3	$10.14 \pm 0.37^{\text{A},\text{b}}$	$11.23 \pm 0.12^{\text{A},\text{b}}$	$14.22 \pm 0.08^{\text{B},\text{b}}$
110 μm Al_2O_3	$10.41 \pm 0.24^{\text{A},\text{b}}$	$11.52 \pm 0.31^{\text{A},\text{b}}$	$15.63 \pm 0.34^{\text{B},\text{c}}$
250 μm Al_2O_3	$11.43 \pm 0.27^{\text{A},\text{c}}$	$13.44 \pm 0.32^{\text{B},\text{c}}$	$16.43 \pm 0.33^{\text{C},\text{d}}$

Table 2. Relative amount of monoclinical phase (%) according to XRD measurements. Same superscript capital letters indicate no significant difference in the same row, and small letters in the same column ($p < 0.05$)

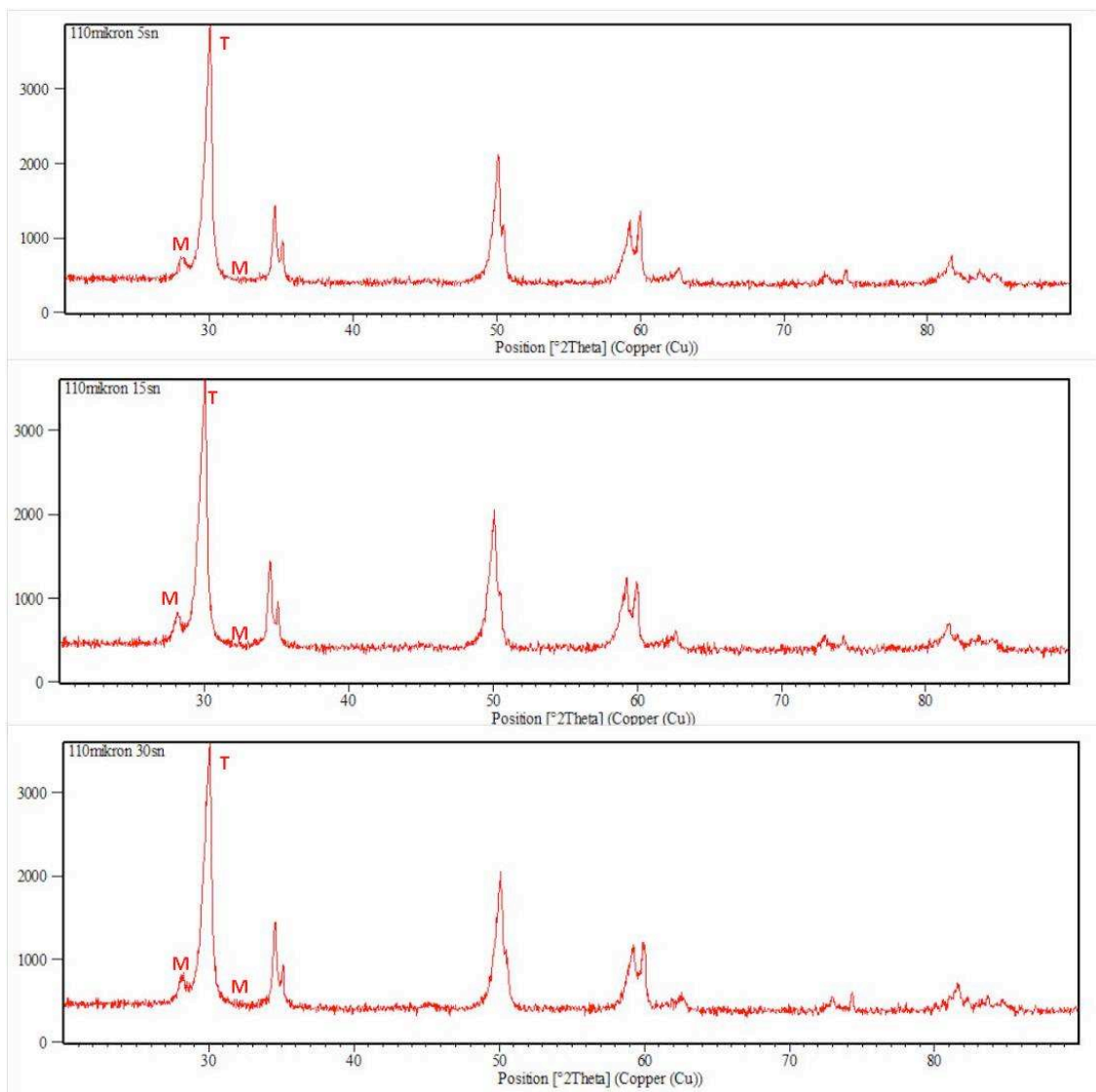
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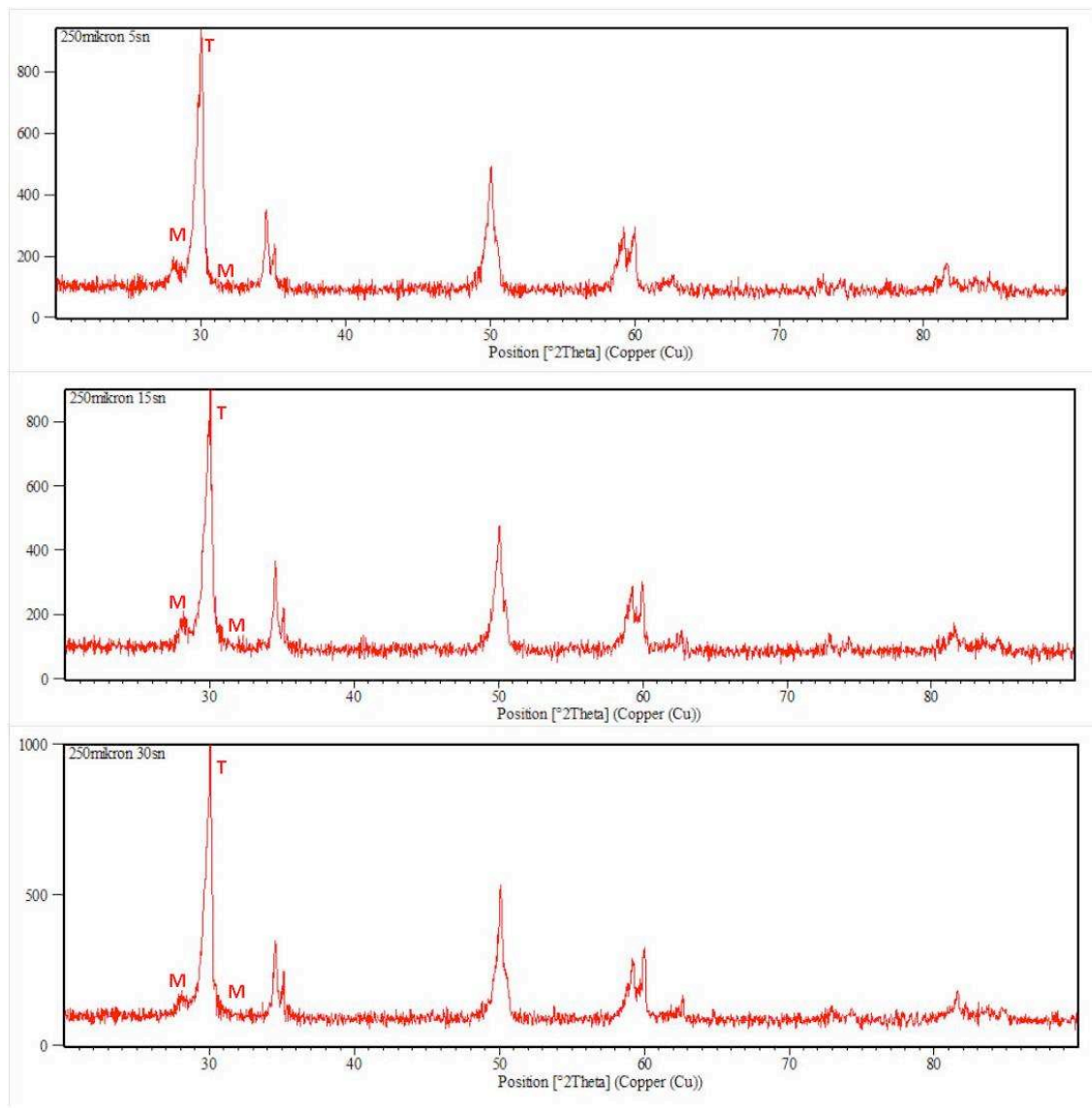
a)



b)

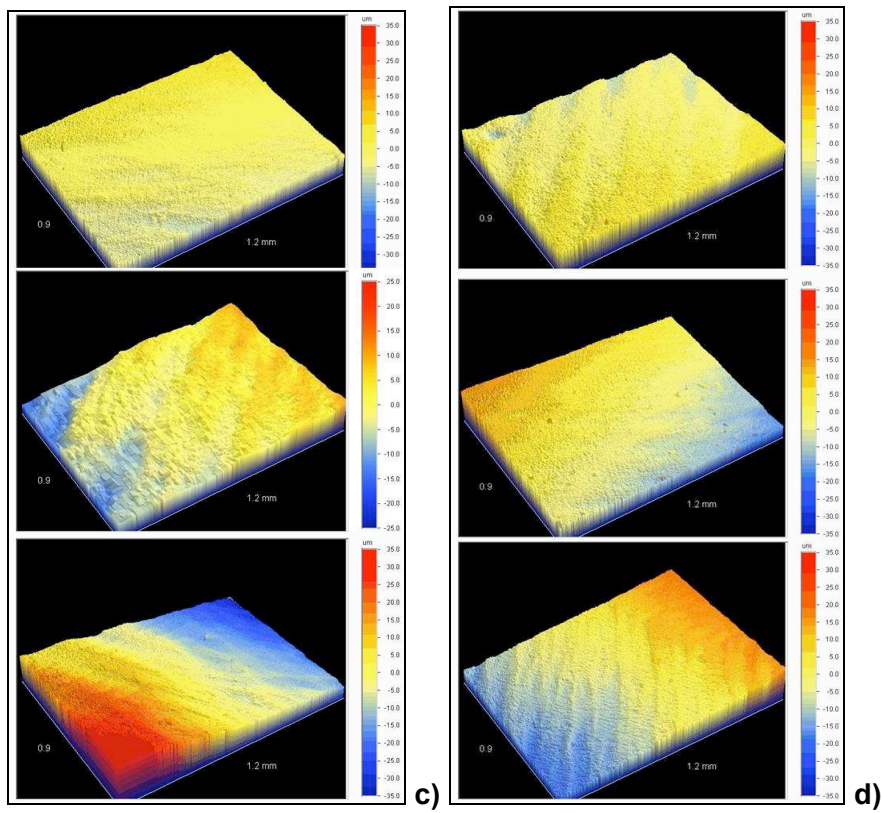
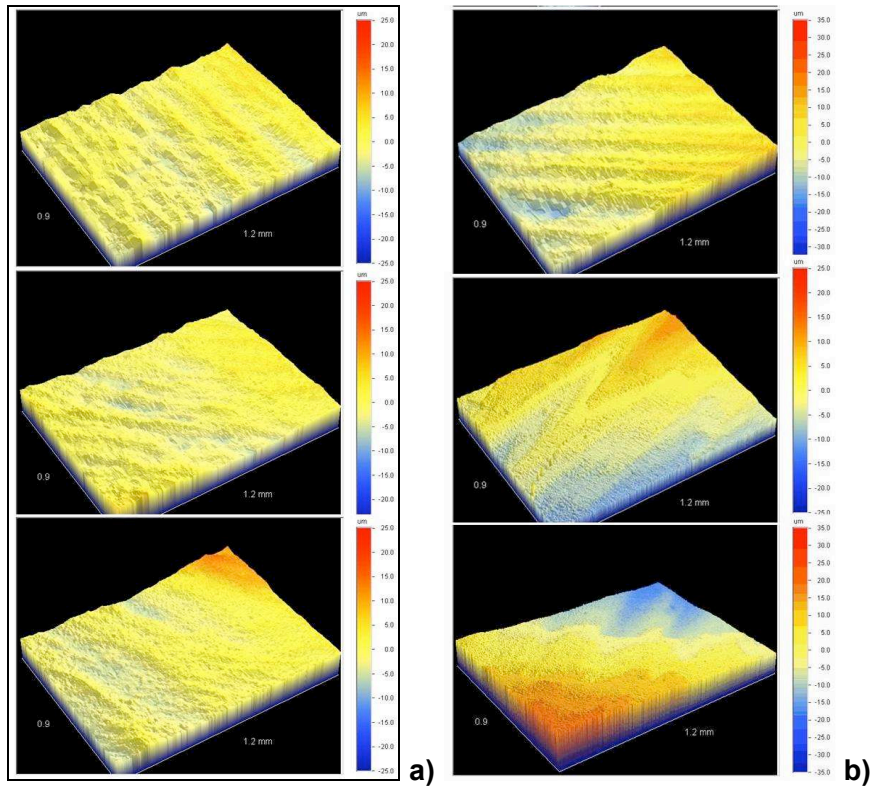


c)

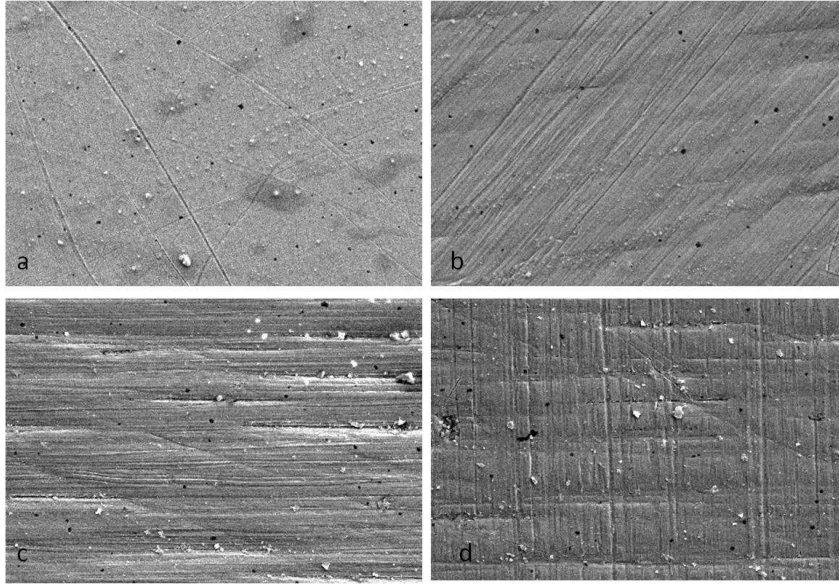


d)

Figs. 1a-d XRD diagrams of zirconia specimens after deposition of **a)** 30 μm SiO_2 , **b)** 50 μm Al_2O_3 , **c)** 110 μm Al_2O_3 and **d)** 250 μm Al_2O_3 for 5, 15 and 30 seconds. **Note the differences in T and M peaks as the application duration changes.**



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Figs. 3a-d SEM images (x700) of zirconia specimens after deposition of **a)** 30 μm SiO_2 , **b)** 50 μm Al_2O_3 , **c)** 110 μm Al_2O_3 and **d)** 250 μm Al_2O_3 for 30 seconds. Note that the hard-milling traces were not completely removed in all groups.